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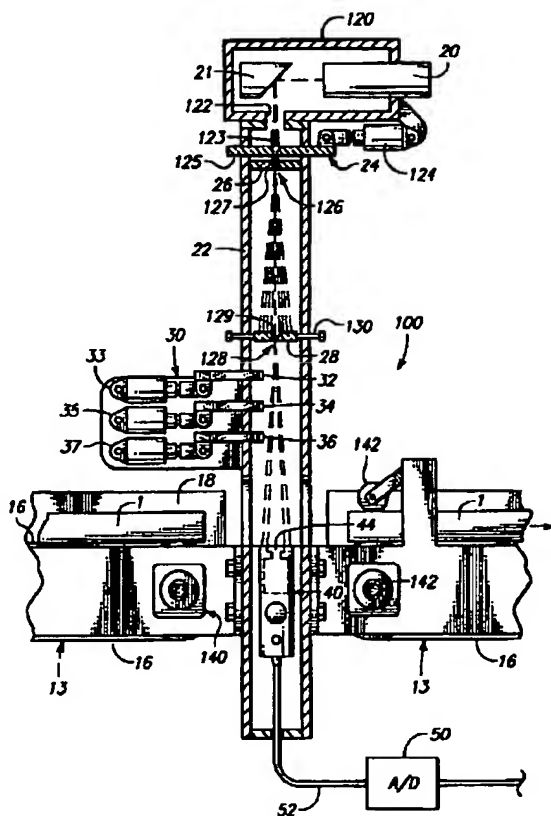
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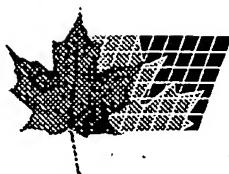
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(54) **METHODE ET APPAREIL POUR UNE MEILLEURE
DETERMINATION DES DEFAUTS PROBABLES D'UNE
PIECE A TRAVAILLER**

(54) **METHOD AND APPARATUS FOR IMPROVED
IDENTIFICATION OF PROBABLE DEFECTS IN A
WORKPIECE**



(57) A method and apparatus for identifying the probable existence and location of defects within a workpiece. The workpiece is preferably wood exhibiting natural variations not the result of defects in the workpiece. The method takes into account the natural variations by segmenting the workpiece into a series of zones. Scanning of the workpiece is performed by an energy source and a detector array. The energy source can be an x-ray source to identify areas of high



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and low density within the workpiece. For each zone scanned, a long-term average of density is determined. Then for each zone a moving average is determined for localized positions, the moving average being a function of the average of density at the localized position and the long-term average. In this way, regional natural variations in the density of the workpiece bias the long-term average of the workpiece. The method can further include the step of smoothing the raw data with a low pass spatial filter to remove noise and natural variation from the energy source and the detector array. The apparatus includes an energy source, a detector array, and a computer configured to implement the method. The apparatus preferably includes an x-ray device having a plurality of calibration shutters which can be used to perform multi-stage calibration of the detectors and the energy source. The x-ray apparatus further includes collimators having chamfered edges in the apertures.

ABSTRACT OF THE DISCLOSURE

A method and apparatus for identifying the probable existence and location of defects within a workpiece. The workpiece is preferably wood exhibiting natural variations not the result of defects in the workpiece. The method takes into account the natural variations by segmenting the workpiece into a series of zones. Scanning of the workpiece is performed by an energy source and a detector array. The energy source can be an x-ray source to identify areas of high and low density within the workpiece. For each zone scanned, a long-term average of density is determined. Then for each zone a moving average is determined for localized positions, the moving average being a function of the average of density at the localized position and the long-term average. In this way, regional natural variations in the density of the workpiece bias the long-term average of the workpiece. The method can further include the step of smoothing the raw data with a low pass spatial filter to remove noise and natural variation from the energy source and the detector array. The apparatus includes an energy source, a detector array, and a computer configured to implement the method. The apparatus preferably includes an x-ray device having a plurality of calibration shutters which can be used to perform multi-stage calibration of the detectors and the energy source. The x-ray apparatus further includes collimators having chamfered edges in the apertures.

**METHOD AND APPARATUS FOR
IMPROVED IDENTIFICATION OF
PROBABLE DEFECTS IN A WORKPIECE**

TECHNICAL FIELD

This invention relates to a method and apparatus for improved identification of probable defects in a workpiece, and in particular to automated high speed linear x-ray lumber grading.

BACKGROUND OF THE INVENTION

It has become a serious consideration in the lumber industry to improve grading of lumber and therefore improve secondary breakdown decisions. By optimizing the recovery of "good wood" against a slate of desired products, the value of the lumber can be increased. "Good wood" refers to wood which meets a prescribed criteria. For different uses, what is considered "good wood" can vary. For example, for fine furniture it may be unacceptable to have any knots in the wood. However, for furniture intended to have a more rustic appearance, a certain number of knots can in fact be desirable. In general though it is desirable to identify certain "defects" in the lumber and to locate them with respect to a spatial reference system. One method of doing this is to have a human visually inspect each piece of lumber prior to it being cut into secondary boards. This is slow and prone to error. Further, even if the defect is identified, the information must still somehow be communicated to a saw operator

1 in a meaningful manner to allow the defect to be isolated, yet allow
2 wood recovery to be optimized against a desired product slate.

3 There have been some improvements in the area of grading
4 lumber, for example Lumber Optimizer (US Patent 4,879,753 to Aune
5 et al) using x-ray, Method of Estimating the Strength of Wood (US
6 Patent 4,941,357 to Schajer) also using x-ray, Dielectric Sensor
7 Apparatus (US Patent 5,654,643 to Bechtel et al) Detector for
8 Heterogeneous Materials (US Patent 5,585,732 to Steele et al) also a
9 dielectric sensing device, and Flaw Detection System Using Microwaves
10 (US Patent 4,514,680 to Heikkila et al) which uses microwaves to
11 measure lumber flaws.

12 Defects include features such as knots, rot, splits, sap, holes,
13 and the like. Defects can be further subclassified, for example a
14 knot can be a sound knot or an unsound knot. Most defects have
15 some attribute which allows them to be detected by automated
16 scanning, for example reflective inspection (laser or gray-scale video)
17 can detect stain and sap in wood. Transmissive inspection techniques
18 (such as x-ray) can detect density variations, and thus knots and rot
19 and the like. However, past efforts to identify defects automatically,
20 particularly with transmissive energy inspection techniques, have met
21 with limited success due to the natural variation in wood density
22 across a board. This is due to the inherent randomness of wood
23 properties, being a naturally occurring, non-homogeneous substance.
Thus, what might appear to an automatic density sensor to be a large

1 area of rot (low density) in a board, might in-fact just be an area
2 of naturally occurring low density within the board.

3 Some past methods of automated lumber grading have had
4 limited success in identifying defects. However, the techniques used
5 often result in more good wood being cut from the board than is
6 necessary. For example, referring to Fig. 1, prior methods might
7 identify the defects 2, 3 and 4 in board 1, but would bracket them
8 with zones 5 and 6, leaving section 9 as waste and only section 7
9 as "good wood." It is desirable if a method and apparatus could be
10 provided which would give the preferred results shown in Fig. 2
11 where the defects 2, 3 and 4 are confined to waste section 11,
12 leaving section 8 as "good wood."

13 In addition to the difficulty of identifying defects and isolating
14 them to a reasonable area within the board, variations in the
15 equipment used to sense the board have contributed to errors in
16 detecting and identifying defects. For example, x-ray scanners, used
17 to measure board density, are inherently "noisy" with scatter, and also
18 tend to "drift" in power output during their warm-up period of
19 operation. Similarly, the sensors or detectors used to measure the x-
20 rays passing through a board are prone to drift.

21 Therefore, what is needed is an improved method and apparatus
22 for detecting defects within a board. Further, there is a need for
23 improved methods of localizing defects once they are detected within
a board to increase yield of "good wood" from the board. There is

1 also a need for an improved x-ray board defect detecting apparatus
2 which accounts for drift and variation in the source and detectors
3 used in x-ray imaging of the board. Preferably, it is desirable to
4 have an x-ray system that allows high speed and accurate lumber
5 grading, improving the location and identification of defects in lumber,
6 thereby improving yield from boards.

7 SUMMARY OF THE INVENTION

8 A method for identifying probable locations of defects within a
9 workpiece is disclosed. The method is particularly applicable to
10 workpieces comprising wood, lumber, or other media wherein a natural
11 variation in a property such as density is found in the medium which
12 can obscure defects which are identifiable by the same naturally
13 varying characteristic. The method comprises the following steps:
14 providing a workpiece to be surveyed for probable locations of
15 defects, wherein the workpiece is capable of being identified by
16 selected regions; providing an energy source which can impinge energy
17 on the workpiece to produce a resulting energy signal indicative of
18 a physical property of the workpiece; and providing a plurality of
19 detectors capable of receiving at least a portion of the energy signal
20 which is produced by the workpiece and generating a detector signal
21 in response to the energy signal. The method includes the step of
22 positioning the workpiece relative to the energy source and the
23 detectors to allow the detectors to receive the resulting energy signals.
In the method the workpiece and the detectors are moved relative to

1 one another while the energy from the energy source is impinged onto
2 the workpiece to produce a series of detector signals which are
3 representative of the physical property of the workpiece at different
4 spatial positions along the workpiece. The detector work signals are
5 stored in a memory device in a manner such that the signals are
6 identifiable by the associated spatial position on the workpiece.

7 The detector signals are processed in the following manner to
8 produce a defect map indicative of the locations and types of probable
9 defects within the workpiece. An average is determined for at least
10 some of the detector signals to generate a bulk average detector signal
11 for the overall workpiece. The bulk average detector signal is then
12 adaptively filtered for selected regions on the workpiece to establish
13 a localized average detector signal, wherein the adaptive filtering is
14 configured to account for variance in the average of the detector
15 signals as compared to the bulk average detector signal. Such a
16 filter can also be known as a "moving average" since the average is
17 adjusted relative to movement along the workpiece. After a moving
18 average for the workpiece has been established, a defect threshold
19 range is established. The defect threshold range is a function of the
20 localized average detector signal (the moving average) such that signals
21 outside of the threshold range can be attributed to a defect in the
22 workpiece. Finally, for at least some of the regions, spatial positions
23 along the workpiece are identified as having corresponding detector

1 signals which are outside of the threshold range, those identified
2 positions corresponding to probable locations of defects.

3 More particularly, the workpiece is divided into a plurality of
4 zones which are oriented in the direction in which the workpiece is
5 moved relative to the detectors. Rather than establish a bulk average
6 for the entire workpiece, bulk averages are established zone by zone.
7 This reduces the effect that a variance in a physical property such
8 as density across the workpiece will have on the bulk average.
9 Moving averages are established for each zone rather than for the
10 overall board. Likewise, defect thresholds are established for each
11 zone rather than for the overall board. In the step wherein the
12 signals are compared to the threshold, defect thresholds between
13 adjacent zones are interpolated to account for variations in physical
14 property across the workpiece. For those zones which are adjacent
15 to an edge of the board, the defect threshold is extrapolated to the
16 edge of the workpiece.

17 The method can further include a step of smoothing the detector
18 signals prior to establishing the long-term average. The step of
19 smoothing the signals is performed to reduce the effects that noise
20 and inherent signal randomness can have on the data. Smoothing is
21 accomplished by filtering the raw data. The filter can comprise a
22 3 x 3 low pass filter wherein the gain and offset are determined by
23 obtaining detector readings with the detectors first fully exposed to an

1 energy source, and then isolated from the energy source to establish
2 a two-point gain/offset correction (respectively).

3 The invention also includes an apparatus for performing the
4 above-described method. The apparatus comprises an energy source to
5 impinge energy on a workpiece, detectors configured to detect energy
6 signals resulting from the impinged energy on the workpiece, a
7 mechanism for causing relative motion between the workpiece and the
8 detectors, and a computer having a memory configured to store the
9 detector signals and to perform the steps of the described method.

10 The invention further includes a computer readable medium
11 having computer executable instructions for performing the described
12 method.

13 The invention also includes an apparatus for projecting an energy
14 beam onto a workpiece. The apparatus is preferably used to perform
15 the above-described method. The apparatus for projecting an energy
16 beam comprises an energy conduit to which at a first end is attached
17 an energy source. Energy from the energy source can exit at a
18 second end of the energy conduit. The apparatus further includes a
19 first aperture device for collimating energy from the energy source
20 into the energy conduit. The apparatus also includes a plurality of
21 calibration shutters, each of the calibration shutters being configured
22 to be operably positionable within the energy conduit to intersect
23 energy within the conduit and produce an attenuated energy beam
which can be impinged upon a detector array.

1 The apparatus preferably further includes a second aperture device
2 disposed within the energy conduit between the first aperture device
3 and the plurality of shutters. The apparatus can further comprise a
4 primary shutter disposed within the energy conduit between the energy
5 source and the first aperture device to allow energy produced by the
6 energy source to be isolated from the energy conduit. The apparatus
7 may further comprise a plurality of detectors held in selective position
8 a distance from the energy conduit outlet, and is further provided
9 with a detector aperture device to focus energy from the energy
10 source onto the detectors. Preferably, the aperture devices comprise
11 a plate having a hole disposed therethrough to act as the aperture,
12 wherein the edge of the hole is chamfered on the side of the plate
13 which is facing the energy source.

14 The invention provides other advantages which will be made
15 clear in the description of the preferred embodiments.

16 BRIEF DESCRIPTION OF THE DRAWINGS

17 Preferred embodiments of the invention are described below with
18 reference to the following accompanying drawings.

19 The invention will be better understood by reference to drawings,
20 wherein:

21 Figure 1 is a plan view of a board showing defects and how defects
22 can be cut away from the board.

23 Figure 2 shows the board of Fig. 1 but with a preferred defect
removal schedule to increase yield of "good wood" from the board.

Figure 3 is an isometric schematic diagram showing a modern lumber mill and the system for determining the presence of defects in a board and making optimization decisions based thereon.

Figure 4 is a side elevation view of a preferred embodiment of an x-ray scanner which can be used to detect defects in a workpiece.

Figure 5 is a schematic plan view of a board defect image map showing grouped defects.

Figure 6 is a graph showing cross-board density variations.

Figure 7 is a plan schematic diagram of a board model segmented into zones for localized long term average density determination.

Figure 8 is a graph showing the moving long term average density variation in a board, the defect thresholds, and two defects.

Figure 9 is a flowchart for performing the method described herein.

Figure 10 is a block diagram of a variation of the system shown in Fig. 3, further including a plurality of sensing systems and a defect assembler.

DETAILED DESCRIPTION OF A PREFERRED EMBODIMENTS OF THE INVENTION

The method and apparatus for automated lumber grading, preferably high speed linear x-ray lumber grading, provides improved identification and location of defects in wood such as rot, knots, sap pockets and voids, and provides higher recovery data (yield of "good wood") for cutting lumber.

Overview of the system

Fig. 3 shows an overview of the system 10 for grading and handling graded lumber, including the cutting of boards, which is generally found in a sawmill or more generally, a plant. Lumber or a workpiece 1 generally advances into the plant from a planer 14 on a feed belt 13 adjacent a fence 18. The workpiece 1 enters a scanner system 100, whereby the workpiece 1 is scanned to detect defects. Although in the present description the invention is described particularly with respect to an x-ray scanner, it is to be appreciated that other types of scanners can also work with the present invention. Although the terms "x-ray" scanner can be used when generally describing the invention, this should not be considered as precluding the use of other types of scanners, particularly when describing the method and apparatus for determining the probable presence of defects in the workpiece. Other types of scanners include, without by way of limitation, a laser scanner, microwave scanners, optical scanners, and computer aided tomography scanners.

When a workpiece 1 enters the scanner station 100 its presence can be detected by a barrier photoeye, although the scanner itself can also be used for this purpose, as will become apparent in the detailed description below. The speed of the workpiece 1 can be tracked using encoder wheels or other means such as a doppler-effect device. Within the scanner 100, image maps (also referred to herein "frames") of the workpiece are collected from the scanner one frame at a time

1 as the workpiece passes through the scanner. The frames are
2 represented by data collected from the scanner which is recorded on
3 a computer readable medium. When a frame has been recorded it is
4 processed and evaluated in a computer system 200 for features and
5 defects of the workpiece. Probable defects are identified, as well as
6 their location on the workpiece, in a data modeler. The data modeler
7 can comprise either the computer system 200, or the host computer
8 330. In a system having a plurality of sensing systems, for example,
9 an x-ray system 100, a profile system 102, and a visual scanning
10 system 104, the data modeler can be replaced with a defect assembler
11 (DFA) 325 as shown in Fig. 10. The defect assembler combines the
12 three models which result from the three sensor systems to produce
13 a more accurate and complete representation of the workpiece. In
14 either case, the resulting data, which is representative of a workpiece
15 such as a board, can properly be described as a "virtual board," since
16 it is a computer model of the board, including those defects which
17 the scanner is capable of identifying. This data representation of the
18 board can also be properly called the "board model."

19 As indicated in Fig. 10, which shows in block diagram form a
20 variation on the configuration of the system shown in Fig.3, the x-ray
21 computer 200 communicates with the rest of the system 10 through
22 a communication system 300 which links together the various
23 components of the system. The system 10 can further comprise a
control subsystem 310 which can be used to track workpieces as they

1 move through the system, and can also be used to control computer
2 controllable saws 400 and 410. The control subsystem 310 can also
3 be used to control a programmable logic control (PLC) device 315
4 which controls field devices such as workpiece routers for routing the
5 workpiece through the system. The system 10 can also include a
6 network server or host 330 which can be used for, among other
7 things, storing the board model and other data, as well as various
8 computer programs utilized by the various other subsystems in the
9 system, on computer readable medium such as a hard drive 332 or
10 a tape drive (not shown). The network server can support
11 human/machine interfaces such as the graphical user interfaces or
12 terminals 340. The network server can also perform other known
13 functions such as communication with remote devices through modem
14 350 (Fig. 3), and interfacing with other computer systems in the mill
15 or other facilities through line 360. For example, the network server
16 330 can provide production information to an accounting or shipping
17 office. It should be appreciated that collection of processors in the
18 overall system 10, including the DFA 325 when used, can be
19 considered as a "computer," even though it is comprised of various
20 components. Alternately, each of the components such as the control
21 unit 310, the DFA 325, the PLC 315, the x-ray computer 200, and
22 the network server 330 can also properly be considered separately as
23 computers. While the system 10 is shown and described herein in
particular configurations in Figs. 3 and 10, it should be appreciated

1 by one skilled in the art that the necessary functions of the
2 invention, as described fuller herein below, can be accomplished with
3 any one of a variety of system configurations.

4 The system 10 further preferably includes an optimizer/decision
5 processor 320, known herein as the "optimizer" for brevity. The
6 optimizer is provided the board model from x-ray computer 200 or,
7 when more than one sensor subsystems are employed, from the defect
8 assembler 325. Based on the board model, the optimizer can make
9 decisions on the best way to cut the workpiece to optimize yield,
10 consistent with the probable existence of defects in the workpiece.
11 The optimizer is more preferably provided with a rule set to compare
12 against the board model, the rule set being a standard by which
13 defects in the board model can be compared to determine if the
14 defect identified in the board model rises to the level where the
15 defect should be excluded from final product. More preferably, the
16 optimizer is provided with a product slate of desired products and
17 quantities. The optimizer can be configured to compare the board
18 model against the product slate to determine if the board can be cut
19 so as to generate a product which is indicated as being required by
20 the product slate. Once a board fitting a product criteria is
21 identified, the product slate can be updated by the control system 300
22 to revise the quantity of product needed to fill a product order. All
23 of the optimizer functions can be accomplished by a computer program

1 or programs. Optimizers and optimizer programs are known in the
2 art and will not be described further herein.

3 Once the optimizer has made a decision regarding a particular
4 workpiece, the decision is preferably communicated to the programmable
5 logic controller 310 for execution. The PLC 310 preferably includes
6 computer readable medium for storing computer programs. Examples
7 of computer readable medium include, without limitation, ROM, RAM,
8 a hard drive, a diskette and diskette drive, a CD ROM and CD
9 drive, a tape and tape drive, and an EPROM. The controller 310
10 can decide whether the board is to be cut or not, and if so, by
11 which saw. Typically a plant has a plurality of computer controllable
12 saws 400 and 410. Such ensures that the sawing of the boards do
13 not become a bottleneck for throughput through the plant. Further,
14 depending on the type of cut to be made (for example, rip or cross-
15 cut), one saw can be preferably configured over the other. Boards
16 can be routed to a selected saw via a conveyor interchange 500
17 which can be for example a pneumatically actuated conveyor
18 interchange system actuated by the controller 310. The conveyor
19 interchanger 500 can move a workpiece from first conveyor 13 to
20 second conveyor 510. The programmable logic controller 310,
21 preferably in conjunction with the network server 330, can track each
22 board as it progresses through the plant.

23 The system 10 is preferably provided with sensors (not shown)
24 to allow the tracking and detection of workpieces as they move

1 through the system. Workpieces can be marked with bar code or
2 other marking as they exit the scanner 100, allowing the board to be
3 tracked as it moves through the plant. For workpieces such as
4 lumber where it can be undesirable to visibly mark boards, bar coding
5 can be accomplished by using ink which can only be read by non-
6 visible light frequencies (such as ultraviolet). Methods and apparatus
7 for tracking workpieces as they move through a plant are known, and
8 will not be describe further herein.

9 In a preferred embodiment of the invention, a workpiece (lumber
10 or a board) is transported through the x-ray scanner or imager 100
11 longitudinally at a relatively high speed (approximately 3.6 meters per
12 second (700 feet per minute) in one example). The conveyor or feed
13 belt 13 can be angled at approximately 20 degrees to the direction
14 of travel of the board to help insure that the lumber keeps in
15 constant contact with the fence 18 as the lumber moves through the
16 scanner 100. Such ensures that a corner reference point for the
17 board remains along a constant, known reference line, being the fence
18 18. As boards enter the x-ray scanner station 100, the feed belt 13
19 can briefly separate at the scanner 100 so as to provide a better
20 image quality, especially when the scanner scans wood species that can
21 cause pitch build up on the feed belt 13.

22 The method for identifying probable types and locations of
23 defects within a workpiece will now be describe in detail, as well as
a preferred embodiment of an x-ray scanner.

Preferred embodiment of an x-ray scanner

Referring to Figure 4, a preferred embodiment of an x-ray scanner 100 is shown. The x-ray scanner 100 can be used with the method and apparatus for defect detection described fuller herein. The x-ray scanner 100 comprises a electron source 20 (which can be described more generally as an energy source) which projects electrons onto a target 21 which in turn generates a stream of photons or x-rays directed towards sensor array 40. Workpieces such as boards 1 are moved by the conveyor 13 into the path of the x-rays. X-rays penetrating the workpiece 1 are detected by detectors or sensors 44. The sensors produce a signal in response thereto which can be recorded or further processed as more fully described below.

The x-ray source 20 is preferably a ceramic x-ray tube assembly or similar type where x-rays are produced and directed by the source 20 towards the sensor array below. A reflector 21 can be incorporated to reduce the height of the apparatus 100. The source 20 and reflector 21 are preferably housed in a box 120 comprising lead to reduce spurious x-rays from escaping. X-rays can exit the box 120 through opening 122 and are projected into the energy conduit 22 towards sensors 44. The conduit 22 can also act as a frame to support the components of the apparatus 100. Directly below opening 122 is a primary shutter 24. Shutter 24 is preferably fabricated from tungsten or similar material resistive to long-term x-ray damage. The primary shutter 24 is provided with an opening 123 to

allow x-rays to pass through opening 122 and into the energy conduit 22. The primary shutter 24 can be translated from side to side by primary shutter actuator 124 to cause the plate 125 to block the stream of x-rays exiting opening 122. Actuator 124 can be a solenoid or a pneumatic actuator. Primary shutter 24 can be used to block the x-ray source from the sensors 44 for purposes such as calibration of the sensors or where it is desirable to isolate the x-ray source from the energy conduit 22 for human health reasons during maintenance of the apparatus 10 and the like. Another purpose for the primary shutter 24 is that the source 20 life expectancy can be lengthened if the power to the source remains on during temporary shut downs when there is no need to shut the power off to the source.

Immediately below the primary shutter 24 within the conduit 22 is a first collimator or aperture device 26. Collimator 26 is preferably fabricated from lead or other similar material impenetrable to x-rays. Disposed through collimator 26 is aperture 126. An exemplary dimension for aperture 126 is approximately 6 mm by 50 mm (1/4 of an inch by 2 inches) to limit the x-rays projected onto the linear detector array 40. First collimator 26 provides a reduction in both scatter and quantity of x-rays projected towards the workpiece. Below the first collimator 26 within the conduit 22 is a second collimator or aperture device 28. An exemplary dimension between the first and second aperture devices is approximately 45 cm (18").

1 Preferably, the second aperture device 28 can be translationally
2 positioned by positioners 130 to allow positioning of the x-ray beam
3 onto the sensors 44. Disposed through collimator 28 is aperture 128.
4 An exemplary dimension for aperture 128 is approximately 2.5 mm by
5 330 mm (1/10 of an inch by 13 inches) to project the x-rays onto
6 a similarly dimensioned detector array 40. Preferably, the top edge
7 of each collimator's aperture 126 and 128 has a chamfer 127 and 129
8 (respectively) to improve scatter reduction of the x-ray beam onto the
9 detector array 40.

10 The sensor array 40 (as well as the x-ray source 20) can be
11 calibrated by exposing the sensors 44 to the x-rays without a
12 workpiece in place, as shown in Figure 4. The x-rays can also be
13 blocked by first shutter 24 to provide a "black-out" reading for
14 calibration. Calibration is desirable due to drift in the intensity of
15 the x-ray source as the source 20 warms up, drift in the response of
16 the detectors 44 due to a variety of factors, and differences in the
17 base response of detectors 44 due to manufacturing variances and
18 environmental conditions (dust on a sensor, etc).

19 More preferably the apparatus is provided with a device allowing
20 intermediate calibration levels beyond fully exposed and no exposure.
21 This can be accomplished by the calibration device 30 shown in Fig.
22 4. Disposed between the second aperture device 28 and the detector
23 array 40 is a multi-stage calibration shutter 30 having a plurality of
calibrations shutters 32, 34 and 36 which can be positioned within the

1 energy conduit 22 to partially block x-rays from the sensors 44. The
2 shutters 32, 34 and 36 are positionable within the energy conduit 22
3 by respective calibration shutter actuators 33, 35 and 37, which can
4 be solenoids or pneumatic actuators. Preferably, actuation of the
5 calibration shutters is computer controlled to allow frequent calibration
6 of the apparatus during a warm-up period, and less frequent calibration
7 thereafter. The shutters 32, 34 and 36 are fabricated from a material
8 which allows passage of an attenuated amount of energy from the
9 source 20 to the detectors 44. In this manner, intermediate
10 calibrations can be accomplished. When three calibration shutters are
11 used as shown, 7 combinations of intermediate calibration can be
12 accomplished. That is, shutters 32, 34 and 36 can be used
13 separately, shutters 32 and 34, or 32 and 36, or 34 and 36 can be
14 used in combination, or all three shutters can be used in combination.
15 This provides for 9 levels of calibration overall (including full-open
16 and fully blocked) for the apparatus 10. Preferably, the shutters 32,
17 34 and 36 are fabricated from a homopolymer polyformaldehyde,
18 known by its trade name is Delrin or other suitable material which
19 allows partial transmission of x-ray energy.

20 The apparatus 100 can be further provided with a detector
21 collimator (not shown) positioned just below the path of the
22 workpieces adjacent the sensors 44. This assists in giving a final
23 reduction in both scatter and quantity of x-rays projected onto the
24 sensor array 40. An exemplary dimension for the aperture in the

1 detector collimator is approximately 2.5 mm by 330 mm (1/10 of an
2 inch by 13 inches). An exemplary dimension for mounting of the
3 detector collimator is about 6 mm (1/4 inch) directly above the
4 sensors 44. This detector collimator is preferably fabricated from lead
5 or tungsten inserted into aluminum or a similar material.

6 The apparatus 100 can be further provided with sensor array 40.
7 In one embodiment, the sensor array 40 consists of 128 individual
8 sensors in a single line where each sensor is approximately 2.5 mm
9 (1/10 inch) by 2.5 mm (1/10 inch). Each sensor can thus be
10 considered as a "pixel". Each sensor is mounted in the path of the
11 projected x-rays and in the path of the workpiece 1, where the
12 workpiece is moved over the array 40 and through the path of the
13 x-rays by conveyor 13 having conveyor belt 16 and conveyor pulley
14 140. The conveyor pulley 140 can further comprise a measurement
15 device 142 such as an encoder wheel for determining the lineal
16 distance that the workpiece 1 has moved past the sensor array 40.
17 The encoder can also be used to determine the arrival of a workpiece
18 by detecting the leading edge of the workpiece as it enters the
19 scanner. This event can then be used to trigger the scanning of the
20 workpiece by the sensor subsystem. In a less preferred embodiment,
21 the workpiece 1 can be temporarily held stationary while the apparatus
22 10 moves over the workpiece. The sensors typically generate an
23 analog signal which can be communicated by signal line 52 to an

1 analog-to-digital (A/D) converter 50. Use of the A/D converter allows
2 the signals to be processed by a digital computer.

3 **Method for determining the probable existence and location in a**
4 **workpiece of defects**

5 Referring to Fig. 3, a workpiece or board 1 enters the x-ray
6 scanner 100 longitudinally and is sensed using the scanner 100. An
7 x-ray scanner as described above is preferably employed to identify
8 defects having density variations. High density defects or variations
9 in a board include knots and compression wood. Low density defects
10 or variations in a board include rot, voids, and large cracks. A
11 detector or sensor array 40 (of Fig. 4) covering the width of the
12 workpiece is preferably used. The signals from the resulting scan are
13 preferably converted to digital signals using A/D converter 50, and are
14 stored in a computer readable memory for further processing.

15 The workpiece or board is preferably scanned in a longitudinal
16 direction such that the major dimension of the board is perpendicular
17 to the detector array and the short dimension of the board (or the
18 width) is parallel to the detector array. The board is oriented in
19 coordinate axes with one corner of the board designated as (x,y) =
20 (0,0). Boards of thickness up to 4 inches may be accommodated by
21 the system described herein. Greater thicknesses can be accommodated
22 with higher powerful energy sources. Preferably, the board is between
23 1 inch and 4 inches thick. Also preferably, the board width is less
than or equal to the width of the detector array.

1 The detectors typically generate an analog signal in response to
2 energy which is transmitted through the board. High density regions
3 in the board will cause less energy to be transmitted, resulting in a
4 lower signal produced by a detector within the detector array. The
5 analog signals produced by the detectors can be converted to a 12-bit
6 digital signal using an analog-to-digital converter. The 12-bit signal
7 can then be provided to a video frame assembler which assembles the
8 data to a line scan configuration. This can be accomplished by an
9 image processing card and a computer. Thus, data from the scan is
10 collected and organized within a computer memory in a configuration
11 such that the 12-bit digital signals are organized with respect to their
12 spatial position on the board in accordance with the (x,y) coordinate
13 system.

14 In a further embodiment of the invention, detector arrays may
15 be oriented radially about the board at 120 degree intervals. Each
16 detector array so provided is preferably provided with its own energy
17 source. In this manner, data may be collected and assembled into a
18 3-dimensional model of the board.

19 Preferably the board is scanned every 2.5 mm (1/10 inch) as
20 the board passes across the detectors. Thus, each 0.1 inch of board
21 scanned may be properly termed as a "line scan." The expression
22 "line scan" will be used herein, and is understood to designate a
23 single transverse scan of the board. Thus, a complete scan of the

1 board is made up of a plurality of line scans as the board progresses
2 longitudinally across the detector array.

3 When the analog signals are converted into 12-bit binary signals,
4 a signal range or pixel value of 0 to 4095 can be achieved. For
5 an exemplary board, an average overall board density of approximately
6 1500 counts is typical. Signals which exceed the normal count by
7 a predefined amount are indicative of areas of high energy
8 transmissivity, indicating the presence of a high density defect such
9 as a knot. Signals which are less than the average count by a
10 predefined amount are the result of areas of low density within the
11 board and are indicative of defects such as rot or a hole.

12 In one example, a sensor array of 128 sensors or pixels spaced
13 approximately 2.5 mm apart is used, for a total scanned width of
14 approximately 32.5 cm or 12.8". Typical board lengths from 4 feet
15 to 20 feet (1.3 m to 6 m) or more can be accommodate by the
16 system. Since the minimum board length commercially encountered is
17 typically no less than 4 feet, a "board" length of 4 feet is used for
18 data processing purposes. An actual workpiece can thus comprise
19 several "board models" of 48 inches. In the following example, it
20 will be assumed that the workpiece is a board approximately 12"
21 wide, although it is to be appreciated that various widths of a
22 workpiece can be accommodated by changing the number of sensors
23 or the sensor spacing. Scanning in the longitudinal direction (the
direction of travel of the workpiece) can be performed every 2.5 mm

(1/10 inch), giving an image of the board of 480 pixels by 128 pixels. The rate of scanning can be performed at 1440 Hz. This provides a signal from the sensors that can be converted to a 12 bit digital signal, allowing a range of 0 to 4095 counts or different density measurements. In the preferred embodiment of the method, a "board" or frame comprises 48" of a first frame plus 4" of the next frame. This provides smooth data continuity from one frame to the next.

The method for identifying the existence and location of probable defects within the workpiece is shown in flowchart form in Fig. 9. The block diagram flowchart 800 can be implemented by reducing each described step to computer program steps to produce a computer program which can be stored on computer readable media and executed by a computer.

In the first step 810 of the method, the workpiece is scanned by passing a workpiece between an energy source and sensors to detect energy transmitted through the workpiece to generate raw data which is preferably converted into 12 bit data by an analog to digital converter to produce a set of signals which will be processed to determine the presence and location of probable defects in the workpiece. Next, in step 820, the sensors or detectors which are used to sense energy transmitted through the board, and the x-ray source are calibrated. Calibration is performed by exposing the detectors directly to the energy source to establish a gain value.

1 The detectors are then completely blocked from the energy source to
2 establish the response of the detectors in the absence of any energy
3 from the energy source which establishes an offset. Then the raw
4 data collected in step 810 is calibrated using a two-point gain offset
5 correction. In the third step 830 the raw data collected in step 820
6 is smoothed using a low pass spatial filter. More preferably, the
7 filter is a 3x3 low pass filter, using the signal established in step
8 820. In step 835 probable defects, known as "candidate objects" are
9 generated using an adaptive thresholding filter, preferably on a
10 longitudinal zone basis, as will be more fully described herein. The
11 resulting product of the candidate object generation step 835 is a
12 series of high density and low density candidate objects and their
13 corresponding location on the board or workpiece.

14 In step 840, the candidate objects are grouped together to
15 "grow" probable defect objects. This is performed by grouping
16 candidate objects identified in step 830 which are within a pre-
17 determined distance of one another. In step 850, a candidate object
18 feature vector is produced. The candidate object feature is extracted
19 from the shape or geometric candidate objects generated in step 840,
20 such as the height, width, aspect ratio, area, and perimeter length of
21 the candidate object. In step 860, the features extracted from the
22 candidate object 850 are compared against a rule-base to reject
23 candidate objects which are unlikely to in fact be defects. This step
can also properly be described as "defect filtering," since the objective

1 is to remove phantom defects. In step 870, the remaining candidate
2 objects are located dimensionally on the workpiece by converting their
3 digital pixel space into spatial (x,y) coordinates which can be provided
4 to a defect assembler and an optimizer for scheduling the cutting of
5 the workpiece into smaller pieces.

6 Each step of the method will now be described more fully.

7 Calibration

8 Due to natural variations in equipment such as the x-ray source
9 and the detectors, which can be introduced by operating temperature
10 and the like, it is preferable to calibrate the detectors based on
11 variances in the energy source and based on their own variation.
12 Typically calibration is performed more frequently early on while the
13 equipment is warming up, and less frequently later. For example,
14 early calibration frequencies of every 5 minutes and later calibration
15 frequencies of every 30 minutes can be used effectively.

16 The image is calibrated using a two-point gain and offset
17 approach by which the value of each pixel (i.e. each of the 128
18 detector pixels) is corrected based on a predetermined fully exposed
19 detector reading (white level) and a fully blocked detector reading
20 (dark level). The detector is fully exposed by taking readings from
21 the detectors when no workpiece or calibration shutter is disposed
22 between the x-ray source and the detector (this is also referred to as
23 the white level correction factor value). The detector is fully blocked
by isolating the x-ray source from the detectors. This is also

referred to as the dark correction value and can also be considered background signal. Calibrated pixel data for real density calibration is generated using the following:

$$v(m)=[y(m)*g(m)]+o(m) \quad (\text{Equation 1})$$

where "m" is the pixel number, "y" is the measured value, g is the gain ("white level"), "o" is the offset ("dark level"), and v is the calibrated pixel value.

Smoothing the Data

The calibrated image is first smoothed using a low pass convolution filter (which is a spatial smoothing filter) which reduces signal noise due to amplification and detector speckle. The use of this type filter is preferable due to its noise removal properties and its ease of implementation. The calibrated image data is preferably smoothed using a 3x3 spatial low pass filter, as follows:

$$v(m,n)=\sum\sum a(k,l)y(m-k,n-l) \quad (\text{Equation 2})$$

where $a(k,l)=1/9$ are the filter weights.

Additional approaches to smoothing the data such as median filters or morphological filters (e.g. dilations and erosions) have also been verified as equally as effective.

Candidate Object Generation and Adaptive Thresholding

Turning to Fig. 6, an exemplary single line scan of a board is shown. The line scan shows the intensity of the count on the

vertical axis and the width across the board on the horizontal axis. It is seen that moving across the board from a position y of 0 to a position y of 12.8 that the count drops from approximately 3200 to 1000. This difference may be the result of natural variation in the density of the wood and not indicative of the presence of a defect. An example of a defect is shown at $y = 7$ inches where the count intensity has risen from approximately 1700 to approximately 2500. The cross-board variation shown in Fig. 6 can also exist in the longitudinal direction of the board. The method preferably is configured to account for the natural cross-board density variation as well as the longitudinal density variation in the board, absent variations due to defects.

Natural cross-board density variation is accounted for by dividing the board into a plurality of zones as shown in Fig. 7 wherein the workpiece one is divided into 6 zones, 401 through 406. Although the number of zones selected is not particularly pertinent, in one example, 10 zones were selected. For each zone then a long-term average in the longitudinal or x direction is determined. The long-term average is then adaptively filtered to obtain a moving average, as will be described further herein. Thus, segmenting the board into transverse zones in the y direction accounts for natural cross-board density variations, while adaptive filtering of a long-term average in the x direction accounts for natural density variations in the longitudinal direction.

1 The adaptive filter adapts the digital signal data to the clear
2 wood density of the board. It is preferable to establish this clear
3 wood density in a first section of the board, for example, in the first
4 meter (36 inches) of the board, to initialize the filter. As shown in
5 Fig. 7, a "board" is defined as being 480 line scans long. When
6 each line scan is 0.1 inch long, this corresponds to 48 inches or 4
7 feet. In fact, the actual length of the board may be longer, but for
8 the data processing purposes described herein, it is preferable to select
9 a single dimension as a defined "board length." The board is divided
10 into frames so that defects can be generated as the board passes
11 through the scanner, and to limit processing of data to a maximum
12 size (for example, 52 inches). An additional benefit of dividing the
13 board into frames is that such allows variable length material to be
14 processed consistently. The frame length is preferably less than the
15 shortest anticipated input material length. Thus, in scanning the
16 board, and in processing the data, a 480 line scan board length is
17 used. Preferably, 40 line scans from the next "board" are
18 incorporated into each board model to allow interpolation and
19 extrapolation of the board model at its end points. Thus, a board
20 model or "frame" of 520 pixels by 128 pixels results.

21 In the first step of the candidate object generation, the initial
22 or starting clear wood density for each cross-board zone is established.
23 It is preferable to establish this initial value within the first 36
inches of the board. The assumption is that the most frequently

1 occurring pixel value will represent the clear wood density of the first
2 several feet of the board. This can be accomplished by assembling
3 a histogram of the pixel counts within the first 36 inches (360 line
4 scans) of a zone and selecting the most frequent pixel value in the
5 histogram. Preferably, the program for selecting the most frequent
6 pixel in the histogram looks only within a certain limit of anticipated
7 clear wood density. If no peak value is found within the selected
8 range, it is indicative of a major defect in the wood or an equipment
9 problem, in which case the clear wood density value from the
10 previous frame is used. The initial piece of the zone which is
11 examined to determine an average clear wood density may be known
12 as the region of interest (ROI). The most frequent value in the
13 histogram is established as the initial or bulk long-term average
14 (LTA_0), and is used to seed the adaptive thresholding filter. LTA_0
15 is calculated for each zone across the board.

16 The next step is to process each line scan in the frame (520
17 pixels x 128 pixels in the example) by first calculating a short-term
18 average (STA) filter value for each zone across the board. The short-
19 term average filter value for a zone is calculated by determining the
20 mean of those pixels in the current line scan of the zone which fall
21 within predetermined upper and lower bounds (upper and lower
22 percentages) of the current long-term average value. Once the short-
23 term average filter value has been determined for a line scan within
a zone, the long-term average is adjusted based on a fraction of the

1 short-term average. This fraction is predetermined by defining the
2 length of the long-term tracking window. The resulting effect is that
3 the short-term filter value for each line scan within a zone biases the
4 long-term filter value either up or down based on whether the short-
5 term filter value is above or below the long-term filter value,
6 respectively. Various schemes can be employed in defining the
7 relationship between the short-term and long-term filters. In essence,
8 this can be viewed as a control system in which the long-term filter
9 is attempting to track the slowly varying density map topology while
10 the short-term filter is providing the feedback as to the direction and
11 rate at which the long-term filter should be moving. The approach
12 employed can be considered a linear feedback loop with hard rejection
13 points. Non-linear or other approaches can be employed based on
14 particular image characteristics or desired result.

15 For the technique employed,

$$16 \quad LTA_{i+1} = LTA_i (f(sta_i)),$$

17 where i is the current line scan, and f is a function. The short-term
18 average can be limited such that it is not greater than nor less than
19 $1.15LTA_i$, for example. This prevents high and low readings from
20 defects artificially driving up or down the clear wood density average.
21 LTA_{i+1} can be properly described as the "long-term moving signal
22 average" for a zone.

23 At this point, the long-term average value has been determined
for each zone for the current line scan being processed. Next, high

and low density candidate object threshold levels are established for each zone based on predetermined high and low density percentages above and below the clear wood density long term average (filter) value, respectively. For instance, high density objects are thresholded (separated) out whenever a pixel is determined to have a value greater than twenty percent (or other predetermined percentage) of the moving clear wood density long term average (filter) value (pixel) value. That is,

$$T_i = LTA_i (1 \pm P),$$

where T is the candidate object threshold count, and P is <1 (preferably $0.5 > P > 0.1$). For example, if a 20% band is established as the threshold, $P = \pm 0.2$, so $T_i = 0.8 LTA_i$ to $1.2 LTA_i$.

The adaptive thresholding is used to separate high and low density candidate objects from the density map. Here the term "candidate object" refers to the fact the object is a candidate (i.e. it has potential to become part of a defect). Typically several "candidate objects" are joined to form a candidate defect object. Candidate objects are separated using adaptive thresholding and are then joined to form candidate defect objects which are then classified as belonging to a specific defect type, as described below.

Linear interpolation is preferably performed between adjacent zone moving long-term average (filter) values in order to remove discontinuities between zones and to better approximate the varying cross-board density. Linear extrapolation is also preferably performed

beyond the mid-point of the first and last zones to better handle the effects near the edge of the board. A piecewise linear interpolation/extrapolation approach was determined to be satisfactory for determining high and low density objects. A polynomial or similar curve fitting approach can also be employed. Each pixel in the line scan is then determined to either belong to a high density object, a low density object, or neither, based on the previously determined high and low density threshold maps (hereinafter referred to as object(s)).

Referring to Fig. 8, a graphical representation of the moving long-term average is shown. Line 180 tracks the workpiece signal density (the actual instantaneous density measured by the sensors). The centerline 160 tracks the moving long-term average LTA_i . Line 162 marks the lower threshold limit TA_L . Pixel values below or less than line 162 are candidates for low density defects. Line 164 tracks the upper threshold limit TA_H . Pixel values above line 164 are candidates for high density defects. An example of a low density defect is shown at 166, while an example of a high density defect is shown at 168. Line 170 is the short-term average (STA) of any given line scan. It can be seen that as the short-term average line 170 moves up and down, the long-term average line 160 generally tracks the motion of the short-term average line 170. Also, during an excursion (166 or 168) the short term average is not generated, and the last LTA is used until the signal returns to within the threshold limits.

The resulting data model may properly be referred to as a density map, a defect map, or a candidate map.

The adaptive thresholding algorithm is summarized as follows:

- Initialize long-term pixel average for each cross board zone if this is the first image frame of the board.

$$r_k = n_{k(max)},$$

where r_k is the k th gray level, n_k is the number of pixels in the image with that gray level, $n_{k(max)}$ is the maximum value of n_k exclusive of background pixel values, and

$$k = 0, 1, 2, \dots, L - 1.$$

- Step line by line through the image frame and perform the following for each cross board zone:
 - Calculate the line pixel average within the cross-board zone.
 - Modify the zone long-term pixel average based on the line pixel average.
 - Calculate the zone low and high density thresholds based on a percentage of the long-term pixel average.
 - Threshold line for low and high density objects (linear interpolation is performed between zones).

The next step is to perform localized joining of similar candidate object types. This is performed using a region growing technique that merges like-candidate objects (high density or low density) that are within a predetermined neighborhood or distance of one another. This is performed in both the width and length directions. Typically several candidate objects will form a high or low density object grouping.

Like candidate (high or low density) objects are joined using

1 local object merging if the distance between adjacent objects is less
2 than a preselected distance. The following is performed:

3 R_i is merged with R_j if $|R_i(x,y) - R_j(x,y)| \leq d$

4 where R denotes a region.

5 Referring to Fig. 5, an example of local object merging is
6 shown. A board model 150 is shown with identified defects. The
7 board model may be considered as an image map or a defect map.
8 Although the board model may be displayed graphically to a user, it
9 can also be stored as a digital representation in a computer readable
10 medium for further processing by the method as described herein. In
11 the example shown, the candidate object generation has identified
12 potential defects 420, 421, 422, 423, 427, 428, and 430. Prior
13 methods of merging defect objects might attempt to merge defect
14 objects 420, 427, 428, 421, 422 and 423 into a single defect bounded
15 by boundary 426. In the preferred method of candidate object
16 merging defects 420, 427 and 428 are merged and surrounded by
17 boundary 424. Defect object 421 may be added to the defect
18 bounded by boundary 424 by increasing the boundary with boundary
19 line 425. Alternately, defect 421 may be isolated to its own defect
20 boundary. It is apparent that bounding defects by boundaries local
21 to the defects decreases the quantity of wood which may need to be
22 removed as waste product. Likewise, prior methods of bounding
23 defect 430 would produce a defect boundary 433 which would result

in loss of area 434. Preferably, defect 430 is bounded by rectangles 431 and 432 thus allowing area 434 to be salvaged as good wood.

The next step is to extract a feature vector from the candidate defect object which will be used to classify or validate the high or low density

objects. Some of the features extracted are the object width, height, pixel area, and aspect ratio of the defect object. Additional features such as the object's average pixel value, elongation, orientation, second and third moments, perimeter length, etc. can also be utilized.

The following features are generated for each candidate object:

- bounding box locations (X_{min} , X_{max} , Y_{min} , Y_{max})
- pixel area (P_{area})
- aspect ratio

The features from the feature vector are then used to either reject the candidate defect object as invalid, in which it is discarded, or to determine the type of high or low density defect detected. The classification approach taken is one of a rule base in which several rules are compared to the generated feature vector. For example, the following criteria is preferably be satisfied:

- minimum and maximum width and height criteria
Width: $(y_{max} - y_{min}) \geq W_{min}$ and $(y_{max} - y_{min}) \leq W_{max}$,
Height: $(x_{max} - x_{min}) \geq H_{min}$ and $(x_{max} - x_{min}) \leq H_{max}$
- minimum and maximum area criteria:
Area: $P_{area} \geq A_{min}$ and $P_{area} \leq A_{max}$
- minimum and maximum aspect ratio criteria:
Aspect Ratio: $(x_{max} - x_{min}) / (y_{max} - y_{min}) \geq R$, and
 $(y_{max} - y_{min}) / (x_{max} - x_{min}) \geq R$

More sophisticated approaches such as using a fuzzy logic and neural networks can also be used. Any candidate objects not rejected are probable defect types, such as rot or knot, that have been detected and classified from the candidate high and low density objects.

Defect objects are then converted from internal pixel unit space to external measurement unit space preferably in thousandths of inches (0.000"). In addition, length (x) and width (y) correction scale factors and offset are applied to correctly reference the coordinate space to some given datum reference. The following conversions are performed:

$$x_{External} = x_{Internal} * x_{ScaleFactor}$$

$$y_{External} = (y_{Internal} * y_{ScaleFactor}) + y_{Offset}$$

In compliance with the statute, the invention has been described in language more or less specific as to structural and methodical features. It is to be understood, however, that the invention is not limited to the specific features shown and described, since the means herein disclosed comprise preferred forms of putting the invention into effect. The invention is, therefore, claimed in any of its forms or modifications within the proper scope of the appended claims appropriately interpreted in accordance with the doctrine of equivalents.

CLAIMS:

1. A method for inspecting a workpiece to determine the probable existence and locations of defects within the workpiece, comprising:

surveying the workpiece with an energy source to generate a response map of resulting signals, the signals being identifiable with locations within the workpiece;

sorting the response map into zones;

determining, for each zone, a bulk average of those signals associated with the zone;

determining, for each zone, a moving long term average for localized positions within the zone, wherein the moving long term average is a function of the bulk average of those signals associated with the zone and the average of the signals associated with the localized position;

establishing a moving defect range for each zone, the moving defect range being within a predetermined percent of the moving long term average for the zone; and

for each zone, identifying those signals which are beyond the moving defect range, such signals being indicative of the probable existence of a defect in the workpiece at the location associated with the identified signal.

1 2. The method of claim 1 further comprising the step of
2 smoothing the signals prior to determining the bulk average of the
3 signals for the zones to remove variations form the signals not the
4 result of variations within the workpiece being surveyed.
5

6 3. The method of claim 1 further comprising, for those
7 identified signals which are beyond the moving defect range, the step
8 of interpolating those signals which are within a predetermined distance
9 of one another and are in adjacent zones.
10

11 4. The method of claim 1 further comprising interpolating the
12 moving defect range between adjacent zones for corresponding positions
13 within the zones.
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1 5. A method for identifying probable locations of defects within
2 a workpiece, comprising:

3 providing a workpiece to be surveyed for probable locations of
4 defects, the workpiece capable of being identified by selected regions;

5 providing an energy source which can impinge energy on the
6 workpiece to produce a resulting energy signal indicative of a physical
7 property of the workpiece;

8 providing a plurality of detectors capable of receiving at least a
9 portion of the energy signal and generating detector signals in response
10 thereto;

11 positioning the workpiece relative to the energy source and the
12 detectors to allow the detectors to receive the resulting energy signals;

13 moving the workpiece and the detectors relative to one another
14 while impinging energy from the energy source onto the workpiece to
15 produce a series of detector signals representative of the physical
16 property of the workpiece at different spatial positions on the
17 workpiece;

18 storing the detector signal in a memory device in a manner such
19 that the signals are identified by the associated spatial position on the
20 workpiece;

21 determining an average of at least some of the detector signals
22 to generate a bulk average detector signal for the workpiece;

23 adaptively filtering the bulk average detector signal for selected
24 regions on the workpiece to establish a localized average detector signal,

1 the adaptive filtering being configured to account for variance in the
2 average of the detector signals near the region compared to the bulk
3 average detector signal;

4 establishing a defect threshold range as a function of the localized
5 average detector signal such that signals outside of the threshold range
6 can be attributable to a defect in the workpiece; and

7 for at least some of the regions, identifying at least some of the
8 spatial positions on the workpiece having corresponding detector signals
9 which are outside of the threshold range, the identified spatial positions
10 corresponding to probable locations of defects.

11
12 6. The method of claim 5 further comprising the step of
13 grouping the identified spatial positions having similar detector signals
14 associated therewith to generate candidate objects, candidate objects
15 being indicative of the presence of a defect in the workpiece.

16
17 7. The method of claim 5 wherein the energy source is an x-
18 ray source of sufficient intensity that at least a portion of the energy
19 may penetrate the workpiece.

20
21 8. The method of claim 5 wherein the workpiece comprises a
22 piece of wood.
23
24

9. A method for identifying probable locations of defects within
a workpiece, comprising:

providing a workpiece having a region to be surveyed for probable
locations of defects, the region having an initial section and a terminal
section, and being characterized by intermediate sections subsequent to
the initial section and prior to the terminal section;

exposing the initial section to an energy source of sufficient
intensity that at least a portion of the energy penetrates the workpiece;

receiving at a plurality of detectors received energy comprising at
least a portion of the energy which penetrates the workpiece at the
initial section, wherein the detectors generate a signal in response to
the energy received thereat;

for at least some of the intermediate sections of the workpiece,
repeating the steps of exposing the intermediate section to the energy
source and receiving at the plurality of detectors the received energy
to generate a plurality of received energy sets corresponding to the
exposed intermediate sections of the workpiece, each energy set having
a section average value corresponding to the average of the signals
generated for the energy set by at least some of the detectors, and
wherein each signal in an energy set corresponds to a spatial position
on the workpiece;

determining an average of at least some of the signals generated
for at least some of sections to establish an overall workpiece average
value;

1 establishing defect thresholds, the defect thresholds being a
2 predetermined percent greater than and less than the overall workpiece
3 average value;

4 determining a moving workpiece average value for at least some
5 of the sections of the workpiece, the moving workpiece average value
6 for a section being a function of the moving workpiece average value
7 for a prior workpiece section and the section average value, wherein the
8 section average value for the initial section is a function of the overall
9 workpiece average value and the initial section average value;

10 determining moving defect thresholds for at least some of the
11 sections of the workpiece, the moving defect thresholds for a section
12 being the predetermined percent greater than and less than the moving
13 workpiece average value for the section to produce a threshold range
14 about the moving workpiece average for the section; and

15 for at least some of the sections, identifying those spatial positions
16 on the workpiece having corresponding signals which are beyond the
17 threshold range, the identified spatial positions corresponding to probable
18 locations of defects.

10. A method for identifying probable locations of defects within a workpiece, comprising:

providing a workpiece having a region to be surveyed for probable locations of defects, the region having an initial position and a terminal position, the region being characterized by a plurality of zones, each zone being defined by a section of the region between the initial position and the terminal position;

providing an energy source of sufficient intensity that at least a portion of the energy can penetrate the workpiece;

providing a plurality of detectors in an essentially aligned configuration, the detectors being capable of receiving the portion of the energy that can penetrate the workpiece;

positioning the workpiece proximate the detectors such that the zones are essentially perpendicular to the essentially aligned detectors, and such that workpiece is disposed between the energy source and the detectors;

moving the workpiece relative to the detectors from the initial position to intermediate positions subsequent to the initial position and prior to the terminal position, and to the terminal position, while exposing at least some of the region to the energy source;

for a plurality of positions of the region, receiving at the detectors received energy comprising least a portion of the energy which penetrates the workpiece, wherein the detectors generate signals in response to the energy received thereat, each said signal being

1 representative of a physical characteristic present at a distinct spatial
2 position on the workpiece;

3 storing the signals in a memory device in a manner such that the
4 signals are identified by zone and by the position within the zone;

5 determining an average of at least some of the signals for at
6 least some of the zones to generate overall zone signal averages for the
7 at least some zones;

8 determining a moving zone average for at least some of the zones
9 of the workpiece, the moving zone average for a position within a zone
10 being a function of the moving zone average for a prior zone position
11 and average of the signals for the position, wherein the position average
12 value for the initial position is a function of the overall zone signal
13 average and the average of the signals for the initial position;

14 determining moving defect thresholds for at least some of the
15 zones, the moving defect thresholds for a zone being a predetermined
16 percent greater than and less than the moving zone average for the
17 zone, the moving defect thresholds defining a threshold range beyond
18 which a signal can be attributable to a defect in the workpiece; and

19 for at least some of the zones, identifying at least some of the
20 spatial positions on the workpiece having corresponding signals which are
21 outside of the threshold range, the identified spatial positions
22 corresponding to probable locations of defects.
23
24

11. The method of claim 10 further comprising the steps of:

exposing the detectors directly to the energy source to generate
a gain;

isolating the detectors from the energy source to generate an
offset;

generating calibrated signals, wherein the calibrated signals are a
function of the gain and the offset;

prior to determining the moving zone average, smoothing at least
some of the calibrated signals by low-pass filtering the calibrated signals
to account for variations in the signals not the result of variations in
the workpiece.

12. The method of claim 10 further comprising, prior to the
step of identifying the spatial positions on the workpiece having
corresponding signals which are outside of the defect range, the step of:

interpolating the moving zone average between adjacent zones to
generate interpolated zone averages, wherein the moving zone average
for zones adjacent an edge of the workpiece are interpolated with one
another; and

using the interpolated zone averages in place of the moving zone
averages to generate the moving defect thresholds.

13. The method of claim 10 wherein signals which are above the threshold range are indicative of areas of high density within the workpiece, and signals which are below the threshold range are indicative of areas of low density within the workpiece, the method further comprising the step of growing candidate objects representative of potential defects within the workpiece, comprising:

grouping identified spatial positions corresponding to signals which are above the threshold range and which are within a predetermined distance of one another to identify high density candidate objects; and

grouping identified spatial positions corresponding to signals which are below the threshold range and which are within a predetermined distance of one another to identify low density candidate objects.

14. The method of claim 10 wherein the signals are analog signals, and further comprising the step of converting the analog signals into digital signals.

15. The method of claim 13 further comprising the step of, for at least some of the candidate objects, generating a feature vector containing characteristics of the candidate objects.

1 16. The method of claim 15 wherein a candidate object is
2 characterized by candidate object characteristics comprising a maximum
3 width, a maximum height, a perimeter length, an area, and an aspect
4 ratio of the maximum width and the maximum height, of the candidate
5 object, and wherein the feature vector for a candidate object contains
6 at least some of the candidate object characteristics.

7
8 17. The method of claim 16 further comprising the step of
9 comparing the feature vectors against a rule base to determine whether
10 a candidate object is likely to be an actual defect, and if so, the type
11 of defect.

12
13 18. The method of claim 10 further comprising the steps of:
14 exposing the detectors directly to the energy source to generate
15 a gain;
16 isolating the detectors from the energy source to generate an
17 offset;
18 generating calibrated signals, wherein the calibrated signals are a
19 function of the signals, the gain and the offset.

20
21 19. The method of claim 18 further comprising the step of
22 smoothing at least some of the calibrated signals by low pass filtering
23 the calibrated signals to account for variations in the signals not the
24 result of variations in the workpiece.

1 20. The method of claim 19 further comprising the steps of
2 disposing a material of known density between the energy source and
3 the detectors, exposing the material to the energy source to generate
4 an intermediate calibration signal, and using the intermediate calibration
5 signal to calibrate the signals.

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7 21. The method of claim 10 wherein the energy source is an
8 x-ray source.
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1 22. An apparatus for identifying defects within a workpiece,
2 comprising:

3 an energy source configured to impinge energy on a workpiece
4 and produce an energy signal in response thereto;

5 detectors configured to detect energy signals produced by a
6 workpiece as a result of energy being impinged thereon by the energy
7 source, and produce a detector signal in response thereto;

8 a mechanism for causing relative motion between a workpiece and
9 the detectors;

10 a computer having a memory configured to store detector signals,
11 the computer being configured to perform the steps of:

12 categorizing stored detector signals based on their associated
13 spatial position on a workpiece;

14 determining a bulk average of at least some stored detector
15 signals to approximate an overall average detector value for a
16 workpiece;

17 adaptively filtering the bulk average to establish a localized
18 average detector signal for selected localized regions on the
19 workpiece, wherein the localized regions are identifiable by spatial
20 positions on a workpiece, and the adaptive filtering being
21 configured to account for variance between an average of detector
22 signals near the region and the bulk average;
23
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1 establishing a defect threshold range as a function of the
2 localized average detector signal such that signals outside of the
3 threshold range can be attributable to a defect in a workpiece;

4 identifying at least some of the spatial positions on the
5 workpiece having corresponding detector signals which are outside
6 of the threshold range, the identified spatial positions
7 corresponding to probable locations of defects; and

8 storing the identified spatial positions in a computer
9 readable medium.

10
11 23. The apparatus of claim 22 wherein the computer is further
12 configured to generate a model of the workpiece, the model identifying
13 the locations of probable defects within the workpiece, the apparatus
14 further comprising a programmable cutting apparatus for cutting a
15 workpiece, the programmable cutting apparatus being configured to
16 receive the model of a workpiece and selectively cut a workpiece in
17 response thereto.

18
19 24. The apparatus of claim 22 wherein the computer is further
20 configured to sort stored detector signals into zones based on their
21 associated spatial position on a workpiece, and wherein the bulk average
22 and the adaptive filtering are performed based on zones.

1 25. The apparatus of claim 24 wherein the computer is further
2 configured to interpolate the defect threshold range between zones.
3

4 26. The apparatus of claim 24 wherein the computer is further
5 configured to interpolate the localized average detector signals between
6 zones.
7

8 27. The apparatus of claim 22 wherein the computer is further
9 configured to:

10 store in the computer memory calibration figures for the energy
11 source and the detectors; and

12 filter the detector signals based on stored calibration figures.
13

14 28. The apparatus of claim 22 wherein the mechanism for
15 causing relative motion between a workpiece and the detectors comprises
16 a conveyor configured to move a workpiece.
17

18 29. The apparatus of claim 22 wherein the energy source
19 comprises an x-ray generator.
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1 30. The apparatus of claim 22 wherein the detectors are
2 configured to produce analog detector signals, and the apparatus further
3 comprises an analog to digital converter configured to convert analog
4 detector signals to digital signals to be received by the computer
5 memory.
6

7 31. The apparatus of claim 22 further comprising a plurality of
8 energy sources in spaced-apart relationship configured to project energy
9 generated by the plurality of energy sources onto a common point of
10 a workpiece.
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32. A computer-readable medium having computer-executable instructions for performing the following steps:

categorizing detector signals stored in a computer readable memory based on an association between a detector signal and a spatial position on a workpiece, wherein a detector signal has a value related to the response of the workpiece as a result of having energy impinged thereon;

determining a bulk average of at least some of the stored detector signals to approximate an overall average detector value for a workpiece;

adaptively filtering the bulk average to establish a localized average detector signal for selected localized regions on the workpiece, wherein the localized regions are identifiable by spatial positions on a workpiece, the adaptive filtering being configured to account for variance between an average of detector signals near the region and the bulk average;

establishing a defect threshold range as a function of the localized average detector signal such that signals outside of the threshold range can be attributable to a defect in a workpiece;

identifying at least some of the spatial positions on the workpiece having corresponding detector signals which are outside of the threshold range, the identified spatial positions corresponding to probable locations of defects; and

1 providing information relating to the spatial positions corresponding
2 to probable locations of defects to a computer-readable memory device.

3
4 33. An apparatus for projecting an energy beam onto a
5 workpiece, comprising:

6 an energy conduit having a first end and a second end;

7 an energy source mounted at the first end of the energy conduit
8 to allow energy generated by the energy source to travel within the
9 energy conduit and exit the energy conduit at the energy conduit second
10 end;

11 a first aperture device for collimating energy from the energy
12 source, the first aperture device being disposed within the energy
13 conduit between the energy source and the energy conduit second end;

14 a plurality of calibration shutters, each said calibration shutter
15 configured to be operably positionable within the energy conduit to
16 intersect energy within the energy conduit and produce an attenuated
17 energy beam at the second end of the energy conduit; and

18 a second aperture device disposed within the energy conduit
19 between the first aperture device and the plurality of shutters and
20 proximate the plurality of shutters.

21
22 34. The apparatus of claim 33 wherein at least some of the
23 calibration shutters comprise a homopolymer polyformaldehyde.
24

1 35. The apparatus of claim 34 wherein each of the calibration
2 shutters allows a different transmissivity of a selected energy type and
3 intensity.

4
5 36. The apparatus of claim 33 further comprising a primary
6 shutter disposed within the energy conduit between the energy source
7 and the first aperture device to allow energy produced by the energy
8 source to be isolated from the energy conduit between the isolation
9 shutter and the energy conduit second end.

10
11 37. The apparatus of claim 33 wherein at least one of the
12 aperture devices comprises a plate having a hole disposed therethrough
13 to allow the passage of energy generated by the energy source, the hole
14 defining a first edge on a first side of the plate, wherein the first edge
15 is chamfered, and wherein the first side of the plate is disposed within
16 the energy conduit such that it is facing the energy source.

17
18 38. The apparatus of claim 33 further comprising:

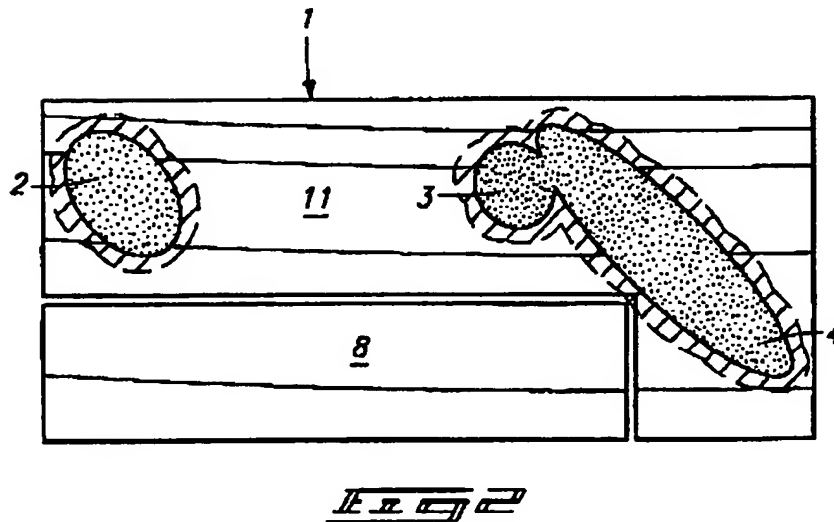
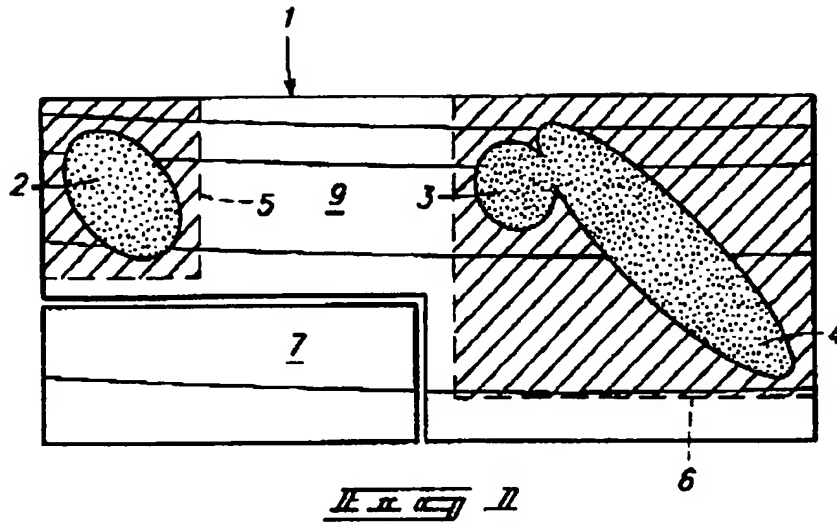
19 a plurality of detectors held in selective position a distance from
20 the energy conduit second end by a detector support;

21 a detector shutter operably positionable between the energy
22 conduit second end and the plurality of detectors to isolate the
23 detectors from energy from the energy source.
24

1 39. The apparatus of claim 33 further comprising:
2 a plurality of detectors held in selective position a distance from
3 the energy conduit second end by a detector support;
4 a detector collimator positioned between the energy conduit second
5 end and the plurality of detectors to focus energy from the energy
6 source onto the detectors.
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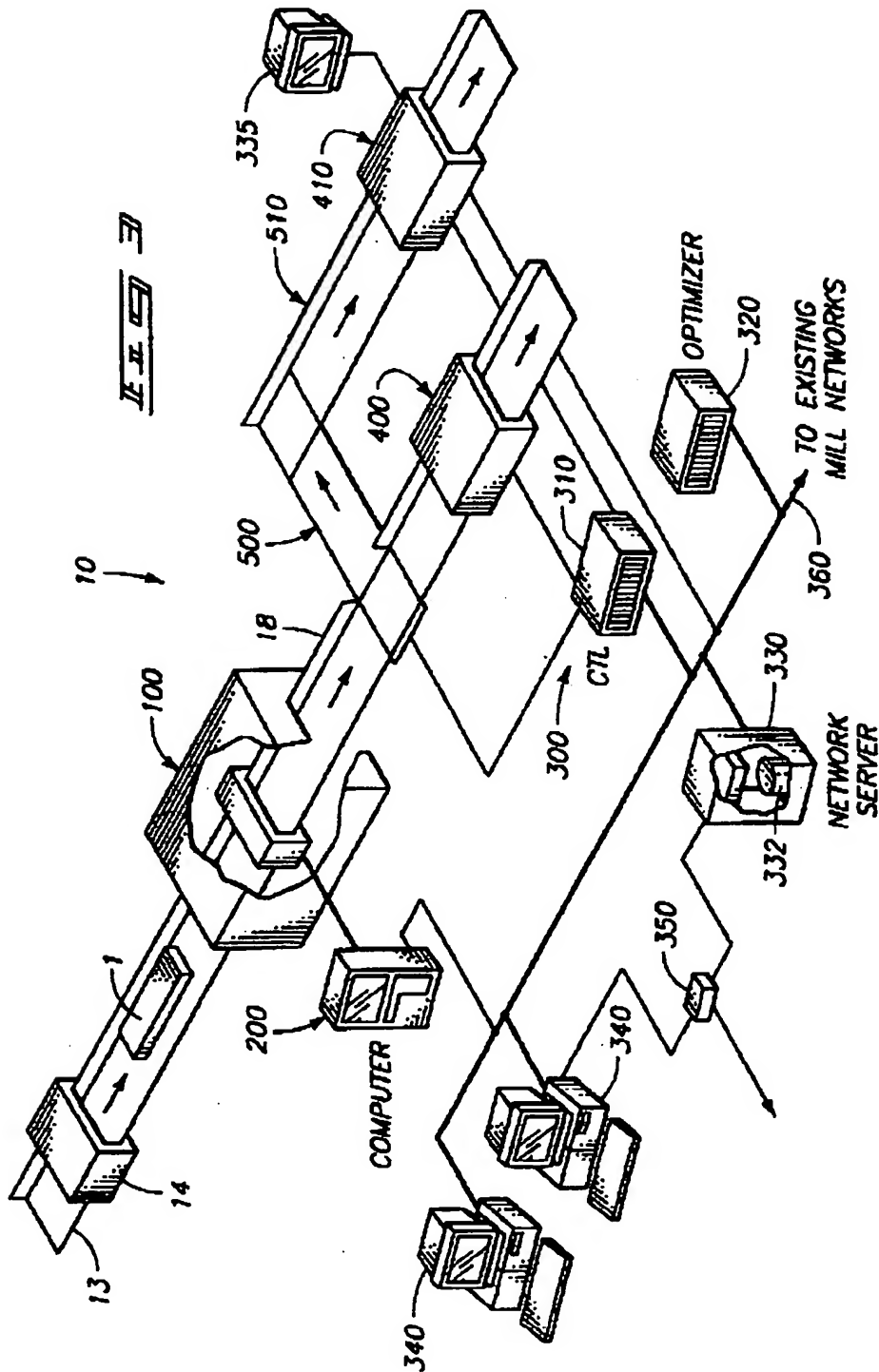
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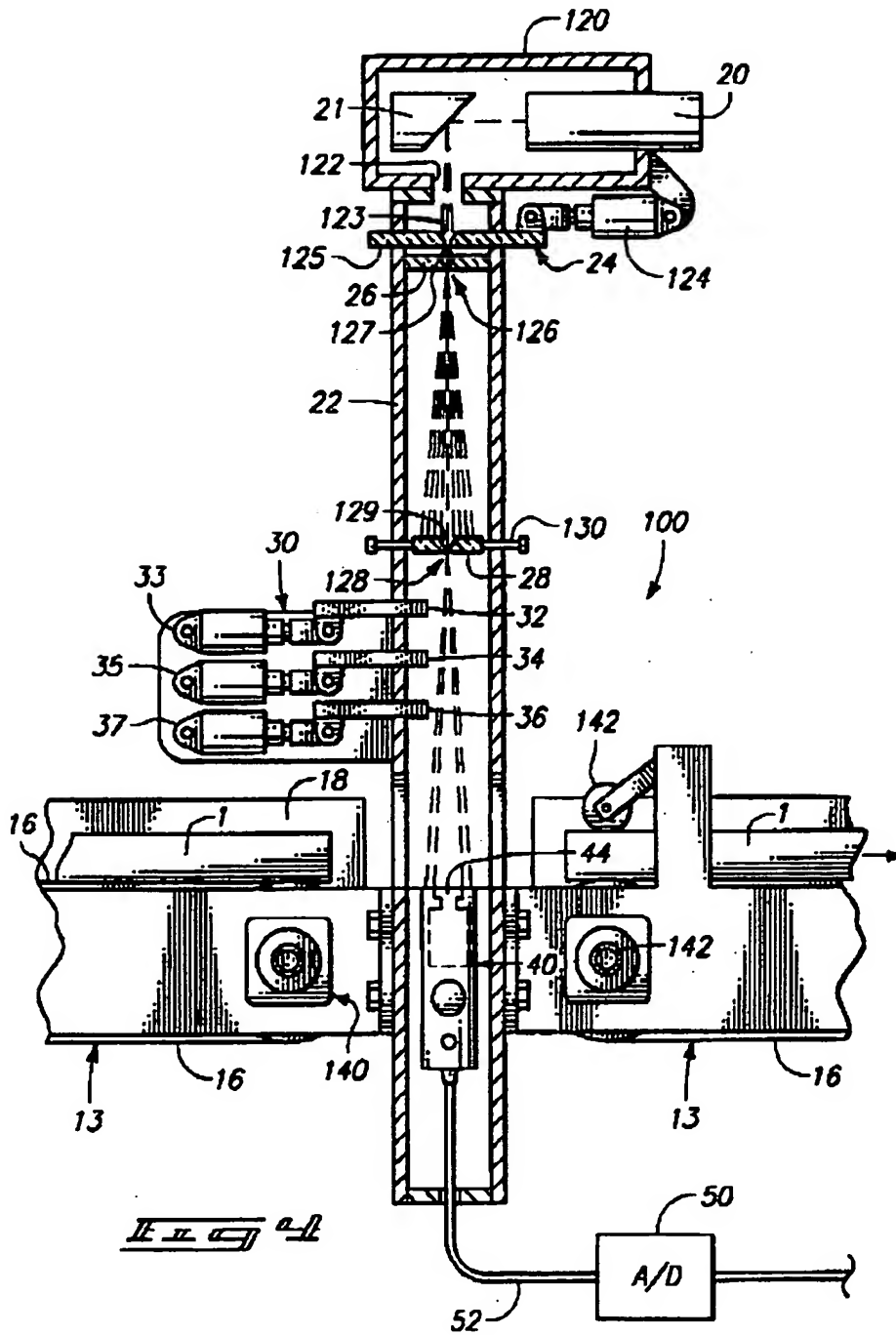
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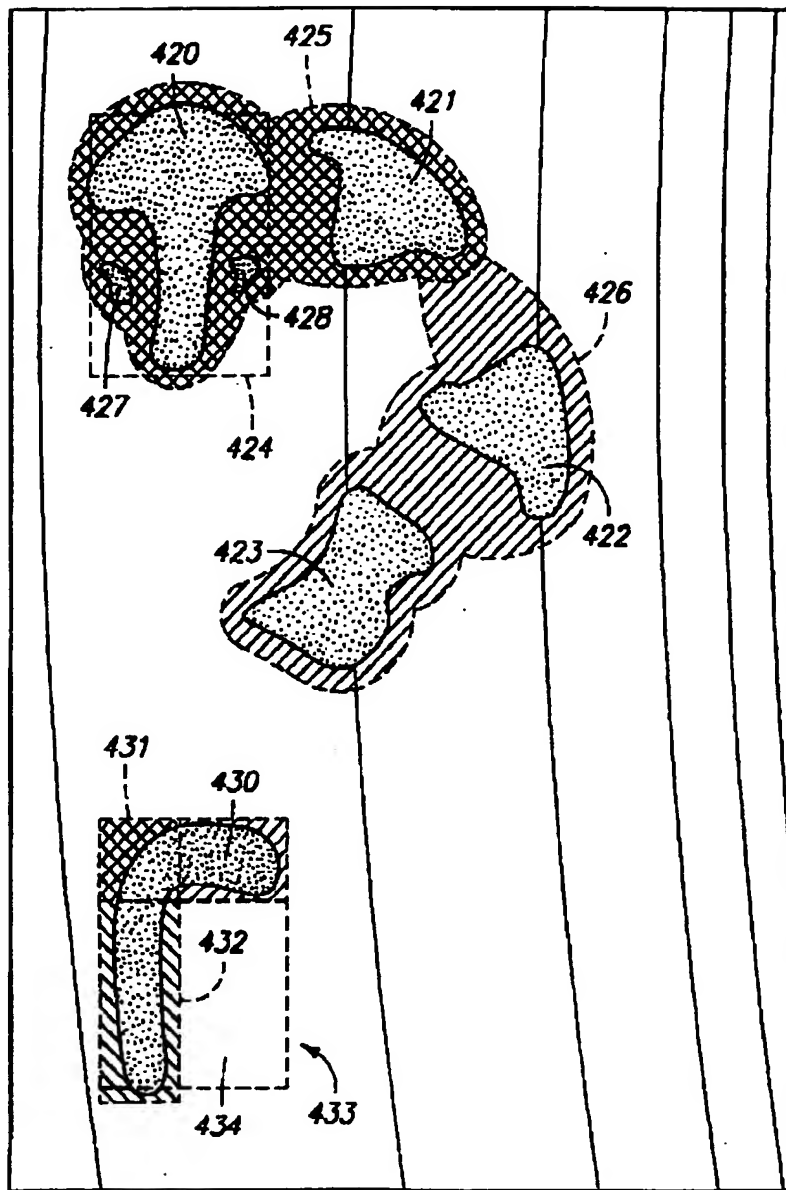
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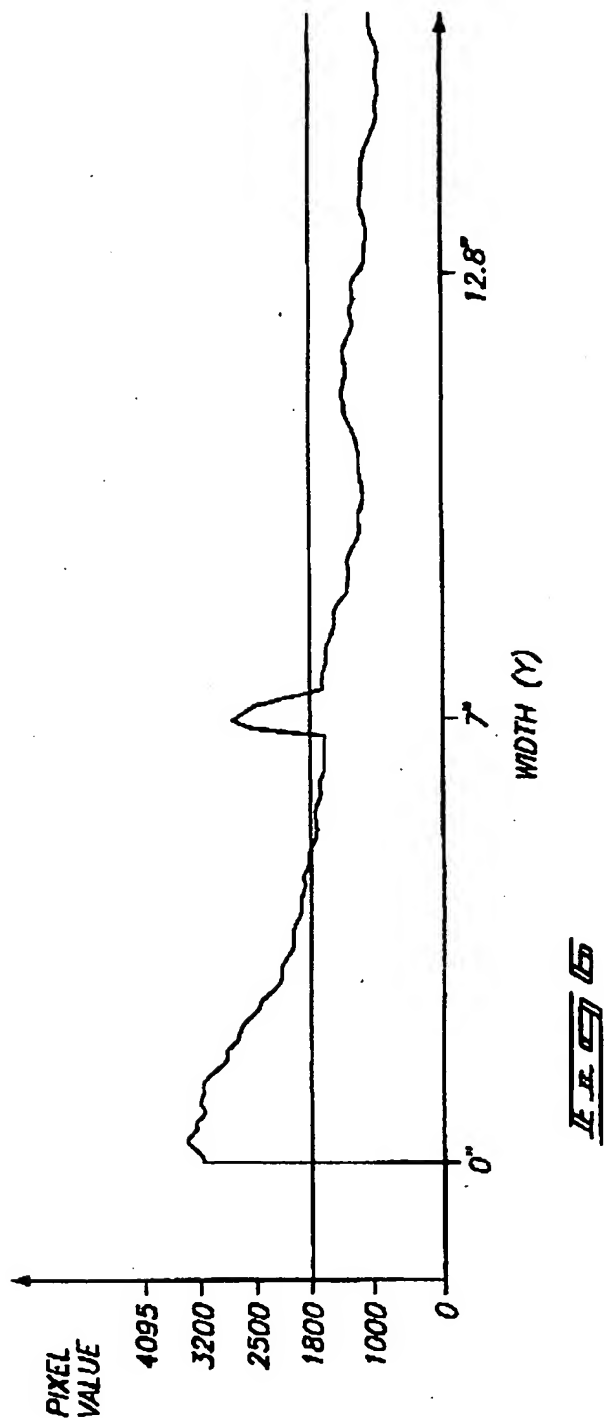


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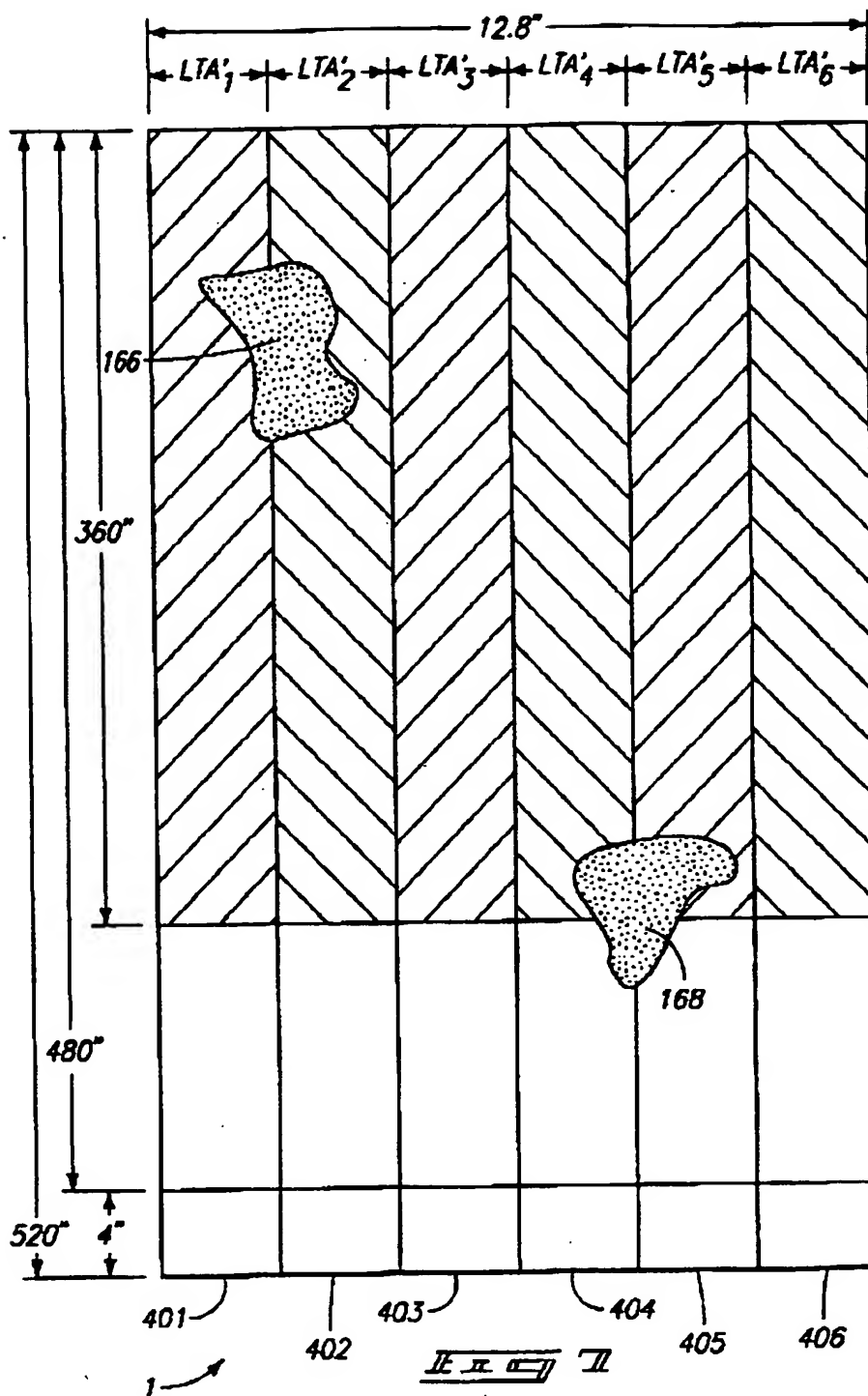
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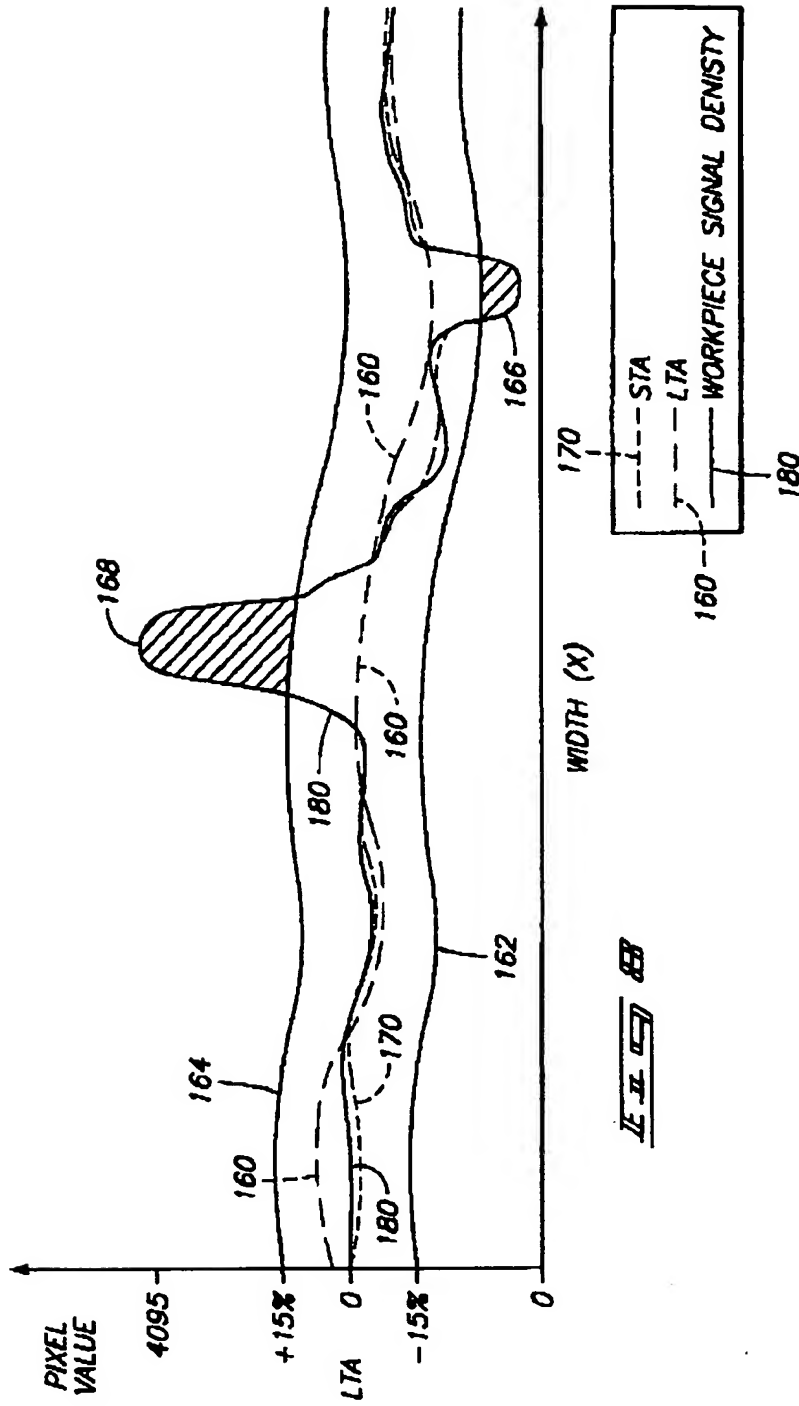


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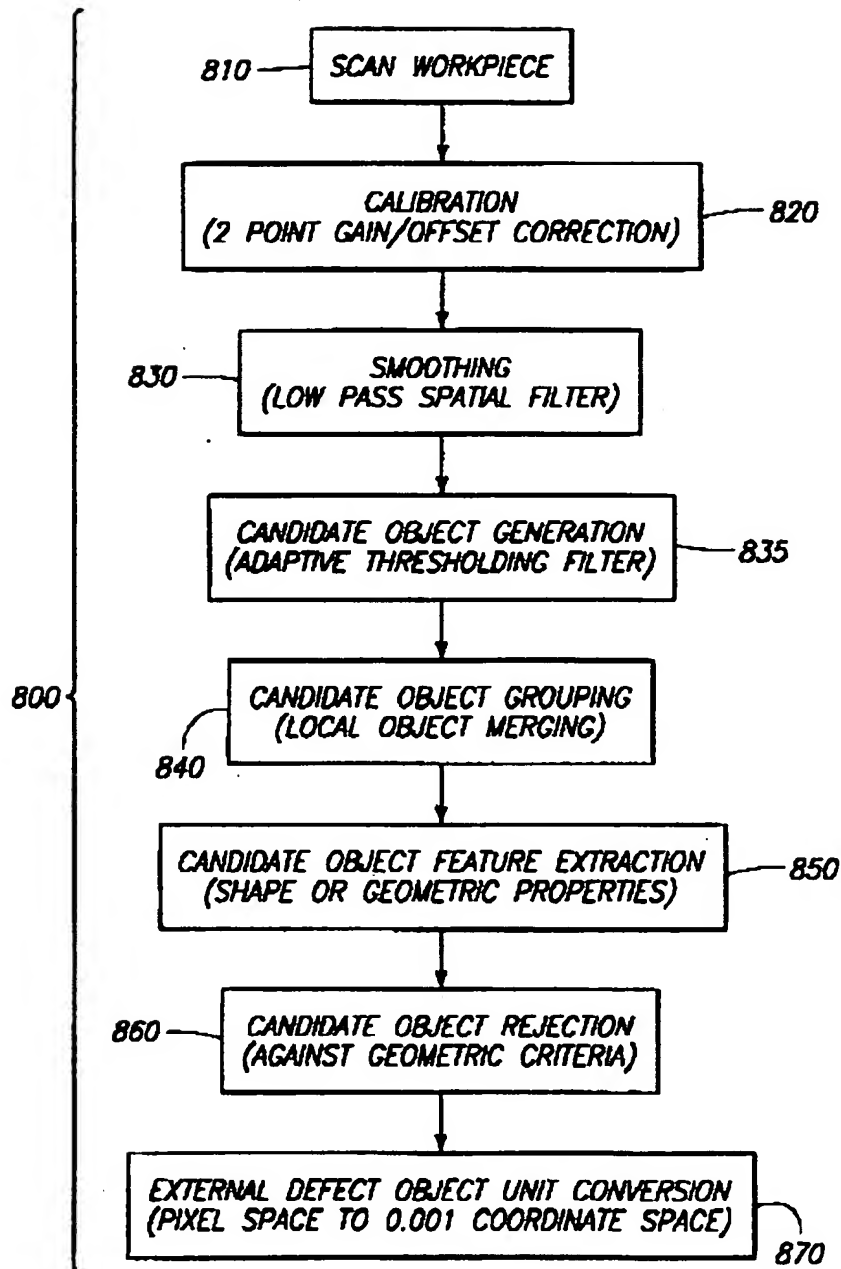
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